

1 **Negative index metamaterial through multi-wave interactions: numerical proof of the concept of**
2 **low-frequency Lamb-wave multiplexing**

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4 Martin Lott¹, Philippe Roux¹, Matthieu Rupin², Daniel Colquitt³ and Andrea Colombi⁴

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6 ¹University Grenoble Alpes, University Savoie Mont Blanc, CNRS, IRD, IFSTTAR, ISTerre, 38000
7 Grenoble, France.

8 ²Hap2U, CIME Nanotech, Grenoble, France

9 ³Department of Mathematical Sciences, University of Liverpool, Liverpool, L69 7ZL, UK

10 ⁴Department of Civil, Environmental and Geomatic Engineering, Institute of Structural Engineering,
11 Swiss Federal Institute of Technology, Zurich, Switzerland.

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13

14 **Abstract**

15 We study numerically the potential of a multimodal elastic metamaterial to filter and guide Lamb
16 waves in a plate. Using a sub-wavelength array of elongated beams attached to the plate, and
17 combining the coupling effects of the longitudinal and flexural motion of these resonators, we create
18 narrow transmission bands at the flexural resonances of the beams inside the wide frequency bandgap
19 induced by their longitudinal resonance. The diameter of the beams becomes the tuning parameter
20 for selection of the flexural leakage frequency, without affecting the main bandgap. Finally, by
21 combination of the monopolar and dipolar scattering effects associated with the coupled beam and
22 plate system, we create a frequency-based multiplexer waveguide in a locally resonant metamaterial.

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25 Introduction

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27 Recent advances in elastic metamaterial design have demonstrated the potential of such
28 metamaterials for the control of wave flow through tuning their mechanical properties at the sub-
29 wavelength scale. Many devices have been successfully tested so far, like lenses [1, 2, 3] or waveguides
30 [4, 5, 6], which have all been based on different physical principles. For example, focusing across a slab
31 can be achieved due to anisotropy and spectral overlap [7, 8, 9], gradient index lenses [3], and coupled
32 resonant modes [10, 11]. Similarly, wave-guides in metamaterials can be obtained through topological
33 insulation techniques [12] and nonlinear harmonics migration [13], and even simpler, with defect-like
34 lines [14, 15].

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36 In the following, we present a combination of these physical principles to build a particular elastic
37 waveguide; a multiplexer that can spatially filter an incident plane wave into different point-like
38 sources for the A_0 Lamb mode. Such multiplexing is made possible through the overlap of two resonant
39 modes of the unit cell of our metamaterial. The metamaterial is constituted of elongated beams
40 attached to a plate, which can couple with the first antisymmetric A_0 Lamb mode with two types of
41 motions, one longitudinal and one flexural.

42

43 We start by recalling previous results for this metasurface made of closely spaced beams. It was first
44 introduced in 2014 by [16], and it has been studied in many ways since: e.g., with numerical
45 simulations, analytical treatments, and experimental observations [17, 18, 19, 3]. The dominant effect,
46 which is not connected to the spatial configuration of the beams (i.e., ordered vs disordered), is linked
47 to the low quality factor longitudinal resonance of the beams, which creates wide bandgaps and exotic
48 dispersion curves for the first antisymmetric A_0 Lamb mode propagation. On top of this, if the plate is
49 thin enough, the flexural resonance create narrow frequency band perturbation, affecting both S_0 and
50 A_0 Lamb mode. Colquitt et al. [19] proposed an analytical formula for the dispersion curve calculation
51 of the plate + beam system. In this analysis, the wave propagation inside the metamaterial is governed
52 by a set of equations, involving the two Lamb modes S_0 and A_0 in the plate and the two resonances of
53 the beams (longitudinal and flexural). The longitudinal resonance of the beams only interacts with the
54 A_0 Lamb mode, the flexural resonance interacts both with A_0 and S_0 through coupling terms (Eq. 2.1a-
55 c in [19]) The dispersion equation is obtained in a closed form but no effective parameters such as the
56 Young modulus or the Bulk density can be expressed. On the other hand, the flexibility of the model
57 makes it possible to consider or eliminate the flexural motion of the resonators that is essential in the
58 proposed multiplexing design. Figure 1 shows dispersion curves computed from Colquitt et al. [19],
59 with or without the flexural resonance effects (panels (a) and (b)), considering the unit cell parameters

60 defined in Fig. 1c. The A0 and S0 free plate response (without the beams) are depicted in gray in Fig.
61 1a. The bandgap induced by the compressional motion is highlighted by the red background color and
62 the blue curve (Fig 1b) includes the beam flexural resonance effects. Figure 1b highlights that the
63 flexural resonances may have different effects according to the frequency of the plate waves in the
64 metamaterial region. In the passband, they interact with the A0 wave but the coupling term is weak
65 and the A0 wave dominates. In the bandgap, where A_0 mode propagation is forbidden, the flexural
66 resonances generated narrow transmission bands, which creates energy leakage from outside to inside
67 the metamaterial (and vice-versa).

68
69 In the following, we show that the start of the main bandgap is underpinned solely by the beam length,
70 and the frequency position of the narrow leakage inside the bandgap due to the beam flexural
71 resonance is a function of both the beam length and diameter. Based on this observation, we propose
72 here a passive spatial multiplexer with a clear understanding of the physics, controlling the two types
73 of beam resonances with independent geometrical parameters, i.e. length and diameter. It has the
74 potential for mechanical filtering A0 Lamb wave in a narrow frequency band, over a wide range of
75 frequencies. Numerical simulations show that the multiplexer waveguides that result have negative
76 refraction indices. Finally, we show that the geometrical periodicity inside of the multiplexing line
77 strongly influences the efficiency of the transmission through the waveguide, highlighting a Fano +
78 Bragg scattering in play.

79

80 **Theoretical approach**

81

82 Starting with the fully elastic formulation from Colquitt et al. [19], we estimate the consequences of
83 changing the resonators diameter on the main bandgap and on the narrow flexural leakage
84 independently. Results of this analysis are presented in Fig. 2b, in a restricted frequency band including
85 the end of the passband (~ 5 kHz) and the targeted leakage frequency interval (~ 6 kHz). The main
86 bandgap induced by the compressional motion is highlighted by the red background color. The flexural
87 resonances create three distinct narrow bands that leak inside the bandgap, depending on the beam
88 diameter, as highlighted with the dotted square in Figure 2b. Changing the resonators diameter thus
89 has a significant impact on the leakage through the flexural resonance, without affecting the main
90 bandgap.

91

92 These results are used here to build a multiplexer by introduction of local defects into the metamaterial
93 waveguide. These defects are obtained by changing the beam diameter for one line of beams, hence
94 by de-tuning their flexural resonances. In practice, each resonance, either longitudinal or flexural,

95 results in a phase jump at the bottom of the beams. The longitudinal resonance is associated to the
96 up-and-down beam motion that induces a negative apparent density as seen by the plate [Williams et
97 al. 2015, Lott et al. 2019] with a monopolar radiation into the plate. Similarly, the flexural resonance
98 induces a bending momentum at the bottom of the beams and thus a dipolar radiation into the plate.
99 The resulting A_0 scattered field differs substantially depending on the resonators motion.

100

101 The tuned leakage through the metamaterial region represents the association of monopole and
102 dipole resonances, which is crucial to obtain double-negative materials, as is demonstrated herein. In
103 the perspective of further experimental realization with this device, the geometry constrain here may
104 require a 3D printing technic to create the sample, with a resolution on the geometry construction less
105 than 0.1 mm.

106

107 **Numerical simulations**

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109 We used the COMSOL simulation software to study the propagation of the antisymmetric A_0 Lamb
110 mode into a metasurface made of 11×21 regularly spaced beams. The simulation box is depicted in
111 Figure 2a, which includes the beam cluster (Fig. 2a-1) and the absorbing areas (Fig. 2a-2). The source
112 is a plane wave (Fig. 2a-3) that is emitted from the right side of the metasurface region and transmitted
113 through the beam cluster.

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115 For the propagating simulations, the system is discretized using two-dimensional (2D) shell elements
116 to model the plate, and 1D beam elements for the resonators, both of which are available in the
117 structural dynamic toolbox of COMSOL. This strategy greatly decreases the model complexity and the
118 computing time, while preserving the full physics of the system. Using a 2-mm thick plate in the
119 numerical scheme, both A_0 and S_0 are reproduced from 0 kHz to 10 kHz, along with the compressional
120 and flexural motion of the beam. We use the same material and geometry as defined in Figure 3c. It is
121 now straightforward to introduce local changes in the beam diameter (Fig. 1c), the key parameter in
122 this study, without worrying about meshing instabilities that would arise using full 3D finite elements.

123

124 The absorbing boundaries are designed using the approach described in [21], with eight different areas
125 that surround the model zone representing the space-dependent attenuation (which increases
126 exponentially from the boundary of the propagating zone to the end of the simulation box). Finally,
127 the full computation takes approximatively one hour in the frequency domain (around 45 seconds per
128 frequency). This strategy provides a high frequency resolution in a narrow bandwidth, with limited
129 numerical cost.

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Qualitative and quantitative results

We ran three different simulations with varying diameters for the central line of the beam cluster (i.e., the waveguide). The background metamaterial consists of beams with a diameter of 5.5 mm and a length of 61 cm. The central line diameters are 5.2 mm, 5.3 mm, and 5.4 mm for the three simulations. Figure 3 shows the qualitative results of the transmitted intensities here. In the frequency band of 6.0 kHz to 6.3 kHz (subpanels 1 to 3 in Figure 3), each selected diameter (subpanels a to c in Fig. 3) creates a leakage at a very precise frequency, thus realizing a frequency-based selector for the A_0 Lamb mode.

We also compute the apparent transmission coefficient, as well as the effective wavenumber inside this waveguide. Figure 4 shows the overall results for the normalized transmitted coefficient (Fig. 4a) and the effective wavenumber (Fig. 4b). In Figure 4a, the three simulations are normalized by the maximum transmitted intensity in the 6.00 kHz to 6.35 kHz band. At around 6.40 kHz (not shown here), the background array made with 5.5-mm-diameter beams globally resonated, which breaks up the wave guidance along the central line. Below this frequency, the three colors in Fig. 4a (blue, red, black) that correspond to the three above-mentioned central line diameters highlight three separate transmission peaks.

For the wavenumber, we simply determine the wave speed along the waveguide. We select three regions to compute the effective wavenumber around each of the transmitted peaks of the three simulations, as plotted in Figure 4b in a $f - k$ frequency-wavenumber graph. We compute the spatial Fourier transform of the wavefield along the line, and select the propagative wavenumber in the positive y -direction.

The negative slope of the phase speed with respect to frequency can be noted here. With a negative slope in the f - k graph, and thus a negative group velocity, the double negativity typical response of this metamaterial is highlighted. Due to the periodicity of the designed array, we display the calculation of the effective wavenumber on the Brillouin edges ($\Gamma - X$) (Fig. 4b). However, we do not observe any spectral folding after ' X ' here. Note that the $\Gamma - X$ direction (Fig. 4b) corresponds to the the reciprocal space ' y ' direction in Figure 2c.

Also, along with these three detected bands, we compute the spatial-spectral amplitude of the tangential and normal components of the wavefield that propagates along the positive y -direction, for

165 the previously estimated wavenumber. We estimate the horizontal versus vertical motion of the plate
166 through the spatial Fourier transform of both in-plan (h) and out of plane (v) motion of the plate
167 surface. The obtained values are reported in color scale in Fig. 4b. With the ratio u/v (i.e., the tangential
168 vs vertical components), we observe smooth transition between ‘quasi’ tangential waves and ‘quasi’
169 normal ones. This transition was already expected by Rupin et al. [22], who also described the coupling
170 between the two orthogonal Lamb modes of the free plate (A_0 - S_0) in this frequency regime.

171

172 **Discussion**

173

174 Previous analytical studies of such a plate+beam system have highlighted the dependency between
175 the slope of the quasi-flat band induced by the flexural resonance inside the bandgap and the overall
176 geometric properties of the system. In particular, the thickness of the plate substrate [19] influences
177 the emergence of a negative index transmission band. Indeed, if the plate is thin enough, the bending
178 moment induced by the flexural resonance of the beams can add negative mass density, in addition to
179 the negative Young’s modulus induced by the longitudinal resonance inside the bandgap [Williams et
180 al. 2016], and thus yield a negative group velocity [23].

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182 In practical instances, double-negative materials come with high attenuation effects [10]. Here, due to
183 the finite size of the system, our transmission coefficient calculation does not capture quantitatively
184 the reflection magnitude at the plate/metamaterial interface. However, previous experimental and
185 numerical data have demonstrated that leakage of such a flexural resonance inside the wide bandgap
186 induced by the compressional motion of the beams can be easily detected [22, 24]. In the present
187 study, we move our attention to the propagation mechanism along the defect line through the
188 introduction of progressive disorder in the multiplexer geometry, to thus identify the scattering regime
189 in play. The results of such simulations are shown in Figure 4.

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191 The numerical model is similar to that shown in Figure 3b. The disorder is implemented by induction
192 of a small spatial random variation along the waveguide (0-6 mm, drawing from a uniform distribution).
193 For each disorder value, three simulations were run, with calculation of the mean transmitted intensity
194 spectra. The results of these spectra are shown in Figure 5a. With disorder, the transmission peak
195 decreases in amplitude. The mean transmitted intensity integrated on the full frequency band (6160-
196 6240 Hz) is shown in Figure 5b as a function of the disorder, where the error bars represent the
197 standard deviations of the simulation results for each disorder value. It is worth noting that the
198 fluctuations over disorder are stronger at a single frequency than in the integrated frequency band.

199

200 Figure 5c-e (Fig. 5c is the same as Fig. 3b, but at 6195 Hz) shows the intensity map at 6195Hz for three
201 particular values of the disorder (i.e., 0, 2, 5 mm random displacement of the beams). In Figure 5c, the
202 beams are depicted as small circles with a black-to-white color scale as the logarithm of the beam
203 motion intensity, and a green-to-yellow color scale as the normalized transmitted intensity (the norm
204 is the maximal transmitted intensity with 0 disorder, as in Fig. 3). We observe that with increasing
205 disorder, the intensity diffusion across the central line might stop. This result differs from previous
206 experimental studies showing the non-effect of the randomness of the beams positions on the main
207 A0 passband [16]. Here, the spatial ordering is essential in this propagative branch, making the coupling
208 between S0 and A0 Lamb mode possible, from the tangential force in the low spatial frequency regime
209 (low-k values), to the predominance of the bending motion in the high spatial frequencies (high-k
210 values). We conclude that the propagation in this frequency band is due to Bragg dipolar scattering
211 between successive aligned beams, which is highly sensitive to disorder. In the absence of disorder,
212 the combination met the criteria for a one dimensional negative index material, resulting in the
213 negative slope in the f-k representation of Figure 4b.

214

215 **Conclusion**

216

217 We demonstrate here the possibility to model a device that can filter and guide low-frequency Lamb
218 waves in a thin plate using the modal overlap of the flexural and compressional resonances of the
219 beam-like resonators. The frequency position of the flexural resonance where the leakage is observed
220 can be adjusted by acting on the diameter of one line of beams, which does not affect the longitudinal
221 resonance that controls the main bandgap. Building on these results, we model a mechanical wave
222 multiplexer that can select the narrow frequency flexural Lamb mode inside a wide frequency
223 bandgap.

224

225 With the combination of two scattering modes, one monopolar and one dipolar, the resulting effective
226 material has a negative refraction index with fast evolution of wave polarization over frequency. The
227 effects of the randomness of the beam positions on the waveguide efficiency are also evaluated, and
228 these confirm the predominance of a Bragg scattering mechanism of intensity diffusion for the flexural
229 resonance of the beams, in addition to the mechanical constraints at the beam attachment due to
230 compressional resonance inside the main bandgap. These results highlight the strong interplay
231 between hybridization due to local resonance, hybridization between different resonant modes, and
232 Bragg scattering versus incoherent scattering. We believe these results can be adapted to any locally
233 resonant system if the individual resonators overlap in their Fano resonances.

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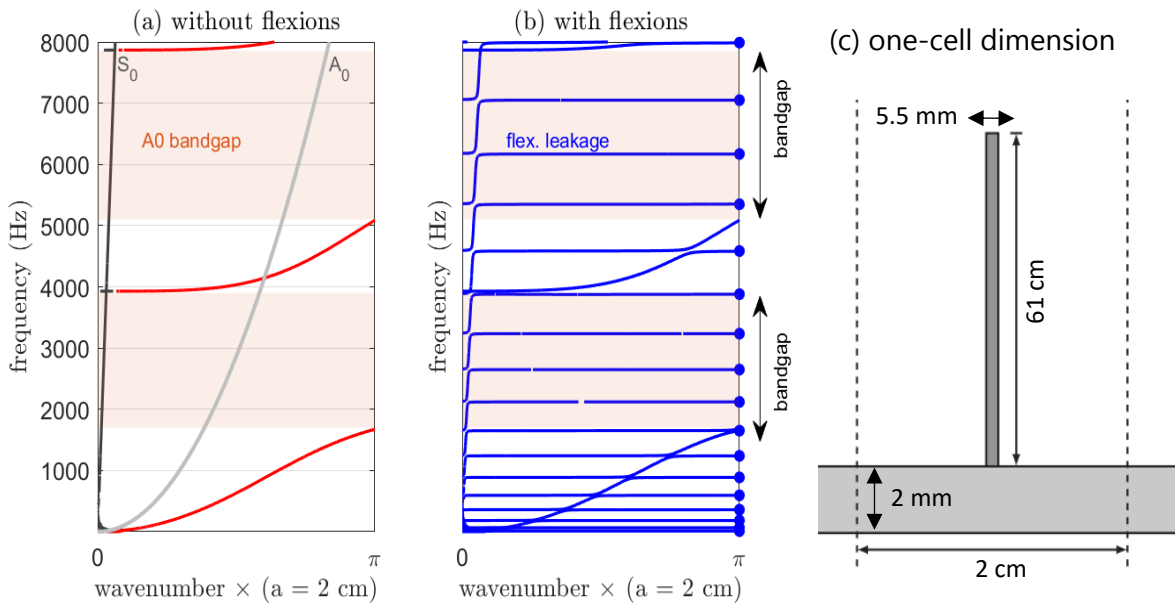
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301 **Figures**

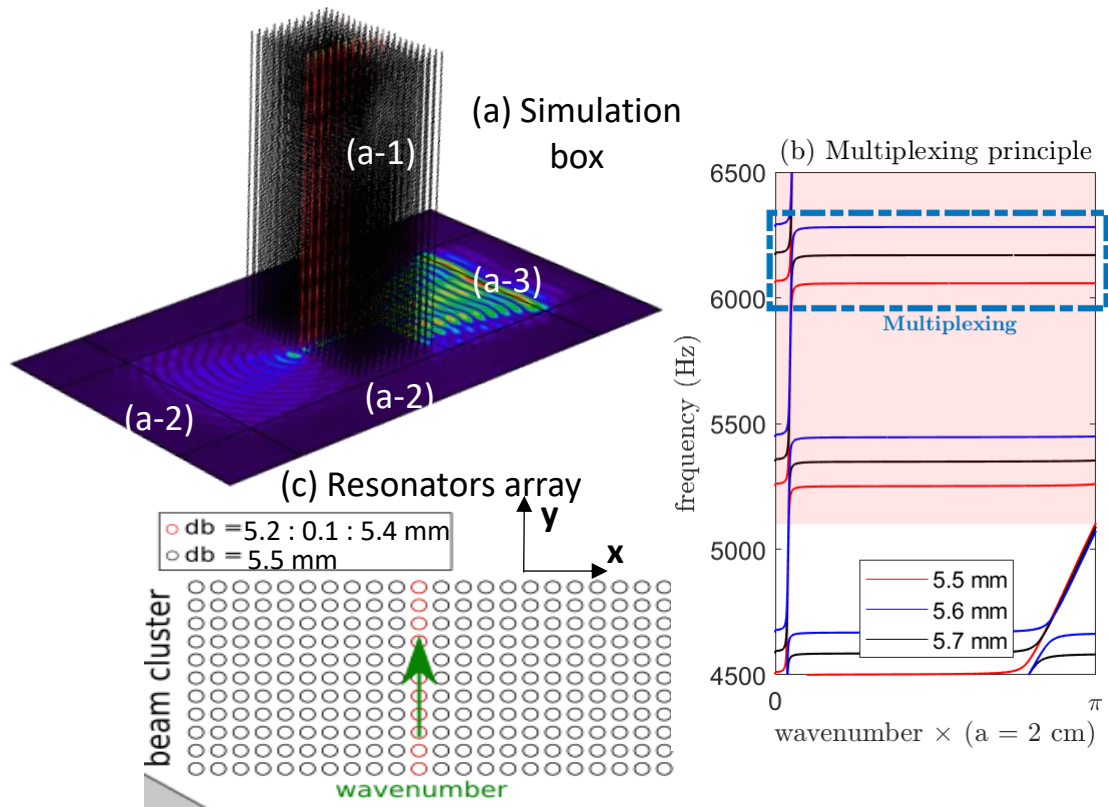


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303 **Figure 1:** Theoretical dispersion relation for an infinite array of beams [Colquitt 2016]. (a) Dispersion
 304 curves obtained neglecting the beam's flexural resonance effects. (b) Dispersion curves with the
 305 flexural resonance effects. (c) Cell dimensions and properties: Lattice constant $a = 2 \text{ cm}$, beam length
 306 $L = 0.61 \text{ m}$, beam diameter $d_b = 5.5 \text{ mm}$, plate stiffness $h = 2 \text{ mm}$ and, aluminum for the material ($E =$
 307 69 GPa , $\nu = 0.33$).

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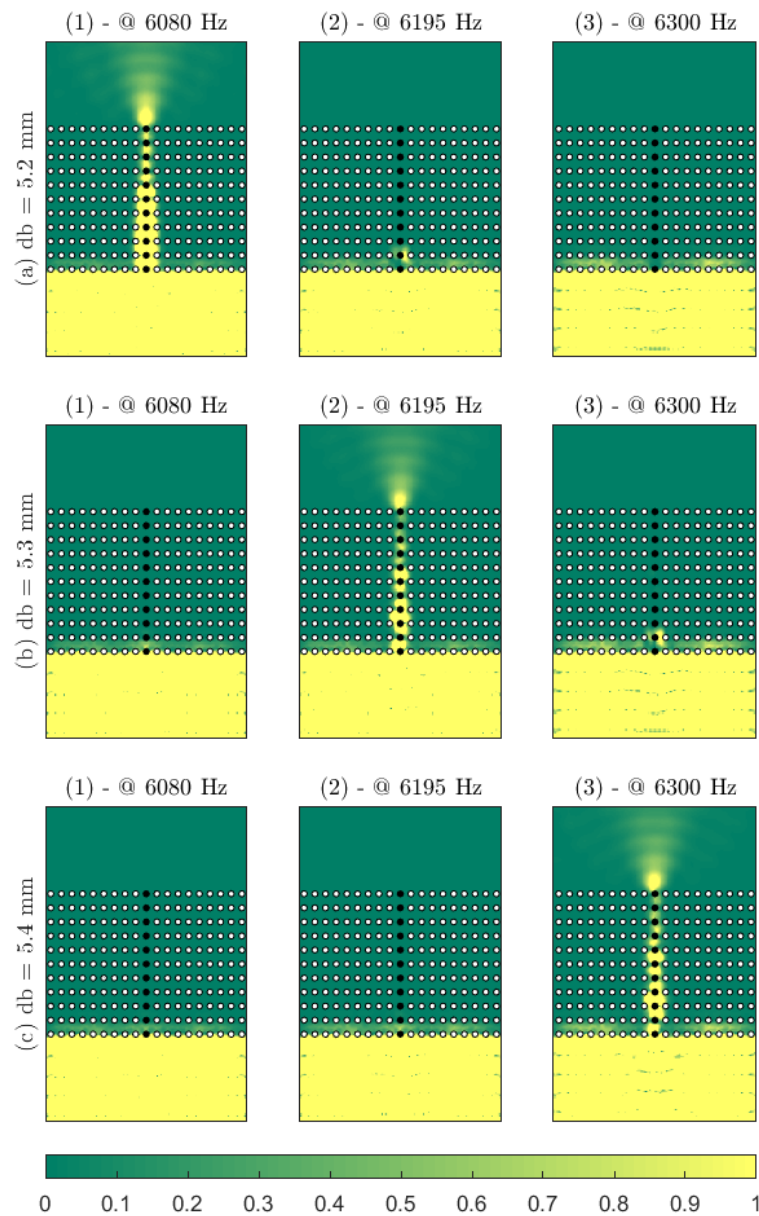


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312 **Figure 2:** Simulation procedure. (a) The metamaterial (a-1) is made of 11×21 regularly spaced beams
 313 attached on a 2-mm-thick plate surrounded by absorbing areas (a-2). A plane wave (a-3) is emitted
 314 from the right side of the beam cluster. (b) Typical band structure for three beam diameters. Inside
 315 the bandgap (redish background area), each flexural resonance creates a different narrow leakage
 316 (dashed rectangle area). (c) Using a different beam diameter along a central line inside the beam
 317 cluster tunes the flexural resonance position without affecting the beginning of the bandgap in this
 318 region.

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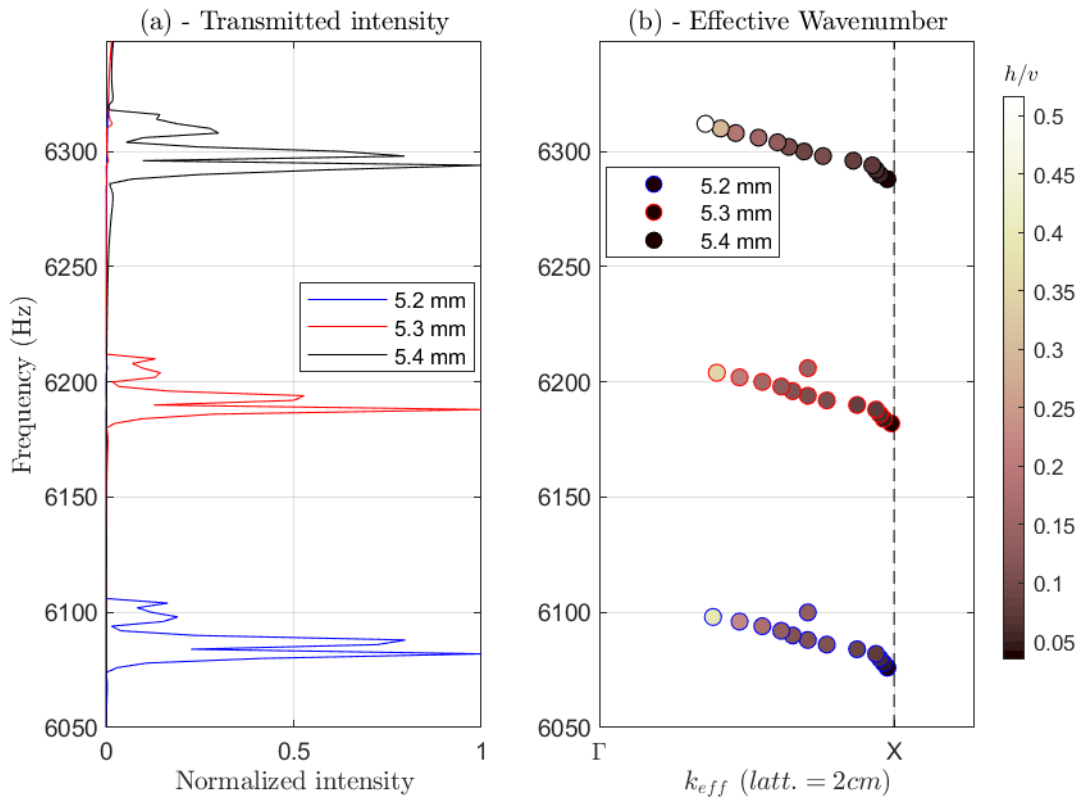


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323 **Figure 3:** Normalized intensity maps for the three-designed waveguides (normalized by maximum
 324 transmitted intensity for each simulation box). The white points represent the 5.5-mm-diameter
 325 beams of the cluster, and the black points indicate the 5.2 mm (a), the 5.3 mm (b), and the 5.4 mm (c)
 326 diameter beams of the central line. From top to bottom (a-c): increasing the beam diameter of the
 327 central line increases the frequency of the flexural resonance and tunes the leakage through the beam
 328 cluster.

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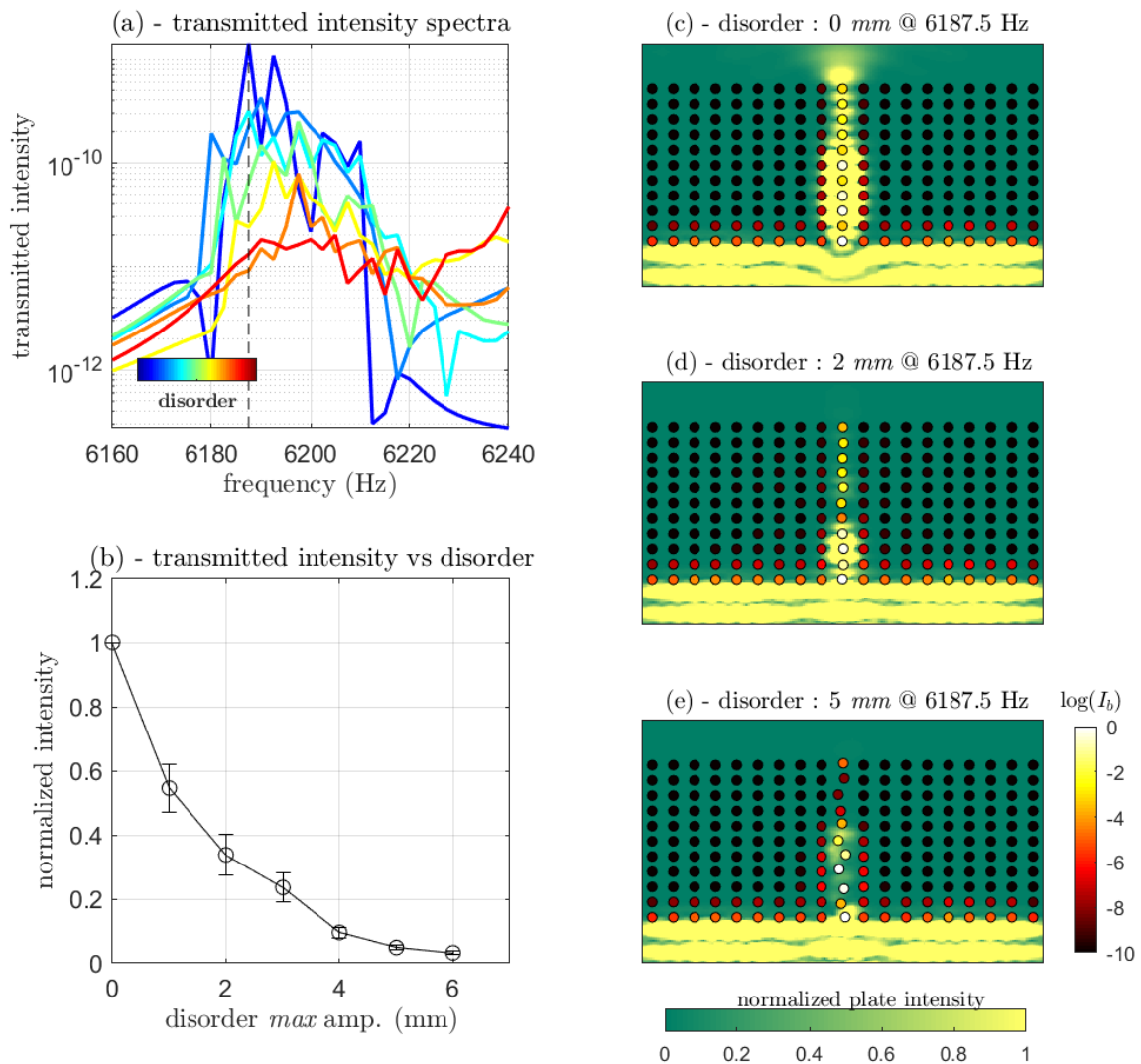


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333 **Figure 4:** (a) Normalized transmission coefficients for the three simulations (blue, red, black) that
 334 create three different leakages. (b) Band structure of the created waveguides (blue, red, black circles).
 335 The color scale in (b) depicts the wave polarization through the u/v ratio (i.e., tangential vs normal
 336 components), computed from the spatial Fourier transform.

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339

340 **Figure 5:** Effects of the randomness of the central line beam positions on the transmission intensity.
 341 (a) Mean transmission spectra for the 5.3-mm-diameter beams in the central line and the different
 342 values of the disorder. (b) Normalized transmitted intensity versus amplitude of the disorder, as
 343 indicated. (c) same as Figure 2b at 6195Hz. (d, e) Intensity map at 6195 Hz for 2 mm and 5 mm random
 344 displacements of the beams in the central line. The intensity maps are normalized by the maximum
 345 transmitted intensity for the case without disorder. (c-e) The beam motion amplitude is depicted as a
 346 'log' scale.